Nonlinear Multi-directional Real-time Hybrid Simulation of Rolling Pendulum Isolation Systems

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# Introduction

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#### Damage to structures due to earthquakes



### Vulnerable non-structural building contents<sup>1</sup>



<sup>1</sup>Casey, Corey D., Rolling-Type Isolation: An Experimental Characterization and Numerical Parametric Study, Masters Thesis, University of Oklahoma, 2017.

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#### Damage to non-structural components<sup>2,3</sup>



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<sup>2</sup>WorkSafe Technologies, Inc., RISK VS ROI, Online, URL https://worksafetech.com/risk-vs-roi/, 2021. <sup>3</sup>WorkSafe Technologies, Inc., PROJECT GALLERY, Online, URL https://worksafetech.com/resources/product-gallery/, 2021.



#### Seismic Isolation



Harvey & Song!

Light (~10<sup>1</sup> kN)!



IHI (https://www.ihi.co.jp/iis/english/products/damper\_floor.html)!



Heavy (~10<sup>3</sup> kN)!

Buckle et al.!



Moderate (~10<sup>2</sup> kN)!



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#### Rolling Pendulum (RP) bearing<sup>4</sup>



Single cabinet configuration

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<sup>4</sup>Casey, C.D., Harvey Jr., P.S. & Song, Journal of Earthquake Engineering. doi: 10.1016/j.engstruct.2018.06.118 GALLOGLY COLLEGE OF ENGINEERING & ENVIRONMENTAL SCIENCE

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## Rolling Pendulum (RP) bearing (cont.)





Coated (QuakeCoat<sup>™</sup>)



Uncoated

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Test set-up

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#### Test set-up

- Single full-scale OCTO-Base<sup>™</sup> isolation system (4 RP bearings) from WorkSafe<sup>™</sup> Technologies (coated and uncoated)
- Shake table NHERI Lehigh EF is mounted on top of a roller bearing bed and free to move and rotate in the plane (X, Y, θ) by means of 3 actuators



South-West top general view





#### Test set-up

- Bottom component of the isolation system is attached to the shake table
- Attached atop: assembly composed of I-beams and a transfer plate, which represents the tributary weight of 17.9 kN (3,850 lb)

Top isolation Bottom isolation system system restraints North view (handling top components)

Top isolation system + Tributary weight



## Test set-up (cont.)

 Top component is restricted from any horizontal movement or rotation by means of 3 restraints attached to the transfer plate



South-East schematic view



## Test set-up (cont.)

- Restraints pinned at both ends
- Uniaxial load cells located at the restraints to obtain directly the experimental restoring force



East schematic view of restraints



## Test set-up: Instrumentation

- Load cells on each actuator and restraint
- Accelerometers on shake table
- LVDTs to measure the horizontal position of the shake table
- Accelerometer and Actuator 5 LVDTs to measure the vertical motion on top **Restraint 3** of the isolation system





Real-time hybrid simulation



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## Set of earthquake records

- ASCE 7-22 Section 16.2 approach for nonlinear response history analysis:
  - Target, 5%-damped, MCE<sub>R</sub> response spectrum was defined for the Los Angeles financial district<sup>5</sup>
  - Deaggregation analysis of the location showed that even though far-field controls FOE hazard, DBE and MCE are controlled by the near-fault events<sup>6</sup>
  - Use of the NGA-West2 database and online tool for amplitude scaling<sup>7</sup>

<sup>5</sup>ASCE, ASCE 7 Hazard Tool, Online, URL https://asce7hazardtool.online/, 2022.

<sup>6</sup>USGS, Unified Hazard Tool, Online, URL https://earthquake.usgs.gov/hazards/interactive/, 2022.

<sup>7</sup>PEER, NGA-West2–Shallow Crustal Earthquakes in Active Tectonic Regimes, Online, URL https://peer.berkeley.edu/research/nga-west-2, 2021.





MCE<sub>R</sub> target response spectrum (near-field without pulse)

## Analytical substructure: SMRF model

- Steel 3-story (LA3) special moment resisting frame (SMRF)<sup>8</sup>
- Inelastic force-based fiber beam-column elements for SMRF's girders
- Elastic elements for remaining structural components
- Modeled in 3D, including P- $\Delta$  effects, using HyCOM-3D<sup>9</sup>



LA3 SMRF model

<sup>8</sup>SAC Joint Venture (2000), *State of the Art Report on Systems Performance of Steel Moment Frames Subject to Earthquake Ground Shaking*, Tech. Rep. FEMA-355C, Washington, DC. <sup>9</sup>Ricles, J., Kolay, C., Marullo, T. M. (2021), *HyCoM-3D: A Program for 3D Nonlinear Dynamic Analysis and Real-Time Hybrid Simulation of 3-D Civil Infrastructure Systems*, Tech. Rep., Hybrid Computational Modeling (HyCoM) Program–3D Version 3.8 User's Manual, Lehigh University.

#### Analytical substructure: **BRBF** model

- Steel 3-story (3vb) bucklingrestrained brace frame (BRBF)<sup>10</sup>
- 3D inelastic truss elements for the BRBs<sup>7</sup>
- Elastic elements for remaining structural components
- Modeled in 3D, including P- $\Delta$  effects, using HyCOM-3D<sup>11</sup>



**3vb BRBF model** 

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<sup>10</sup>Sabelli, R. (2001), *Research on Improving the Design and Analysis of Earthquake Resistant Steel Braced Frames*, Tech. Rep. PF2000-9, Earthquake Engineering Research Institute, Oakland, CA. <sup>11</sup>Kersting, R. et.al. (2015), *Seismic Design of Steel Buckling-Restrained Braced Frames: A guide for practicing engineers*, NEHRP Seismic Design Technical Brief No. 11, NIST GCR 15-917-34.

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## **RTHS** implementation

- MATLAB/Simulink<sup>12</sup> simulation coordinator interface
- Analytical substructure component modeled in customized RTHS software HyCOM-3D<sup>5</sup>, using explicit-formulated computational elements<sup>13</sup>
- MKR-α used as the integration algorithm (model-based, secondorder accuracy, explicit unconditionally stable)<sup>14, 15</sup>

<sup>12</sup>MATLAB and Optimization Toolbox Release R2022a, The MathWorks, Inc., Natick, Massachusetts, United States
<sup>13</sup>Kolay, C. & Ricles, J.M. (2018), *Journal of Structural Engineering*. doi: 10.1061/(ASCE)ST.1943-541X.0001944.
<sup>14</sup>Kolay, C. & Ricles, J.M. (2014), *Earthquake Engng Struct Dyn*. doi: 10.1002/eqe.2401.
<sup>15</sup>Kolay, C. & Ricles, J.M. (2017), *Journal of Earthquake Engineering*. doi: 10.1080/13632469.2017.1326423.
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Simulation coordinator of synchronized control & data acquisition in MATLAB/Simulink<sup>8</sup>

## RTHS implementation (cont.)

- To control numerical dissipation and overshoot, dissipative integration algorithm  $\rho^*_{\infty}$  = 0.5 <sup>14, 15</sup>
- The integration time step was established at 2/1024 s with 2-step interpolations
- Adaptive time series (ATS) compensator essential to actuator control<sup>16</sup>





Input & output disp. servo-hyd. system with experimental substructure relationship<sup>12</sup>

<sup>16</sup>Chae, Y., Kazemibidokhti, K., & Ricles, J.M. (2013), *Earthquake Engng Struct Dyn.* doi: 10.1002/eqe.2294.



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## RTHS implementation (cont.)

 Restraints are equipped with uniaxial load cells to obtain directly and in real-time the experimental restoring forces





Selected results



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#### 3-D Real-time Hybrid Simulation SMRF with RP Isolation System (FIS) @ 2<sup>nd</sup> Floor, Coalinga EQ Scaled to SLE



X-direction = 270 component, Z-direction = 360 component

3-D Real-time Hybrid Simulation of a 3-Story SMRF with 2nd Floor Rolling Pendulum Equipment Isolation System: 1983 Coalinga EQ Bidirectional Ground Motions Recorded at Cantua Creek School and Scaled to SLE Hazard Level.

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#### Equipment Acceleration SMRF with RP Isolation System @ 2<sup>nd</sup> Floor

SMRF 2<sup>nd</sup> Floor Total Acceleration



#### **Equipment Total Acceleration**



| Reduction in Equipment<br>Total Acceleration |             |
|--|-------------|
| X-Direction                                  | Z-Direction |
| 81.3%  | 68.9%       |



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The opinions expressed herein are those of the authors and do not necessarily reflect the views of the sponsors



