NHERI Lehigh Researcher's Workshop: Advanced Simulation for Natural Hazards Mitigation, Lehigh, December 5-6, 2016

MDOF Hybrid Shake Table Testing of Response Modification Devices

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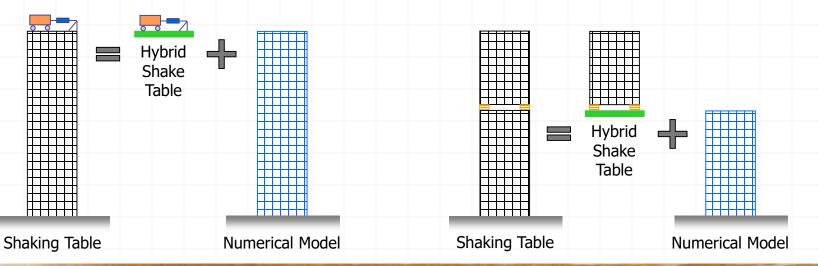
Outline of Presentation

- 1. Motivation
- 2. Hybrid Shake Table Testing
- 3. Stability and Accuracy Considerations
- 4. Test Rehearsal and Safety Precautions
- 5. Bridge Application
- 6. Building Application
- 7. Summary & Conclusions



Motivation

- Many structures exhibit significant rate of loading effects
- Need testing to occur at or near real time
- Large systems such as tall buildings, longspan bridges, or SFSI are difficult to test on shake tables

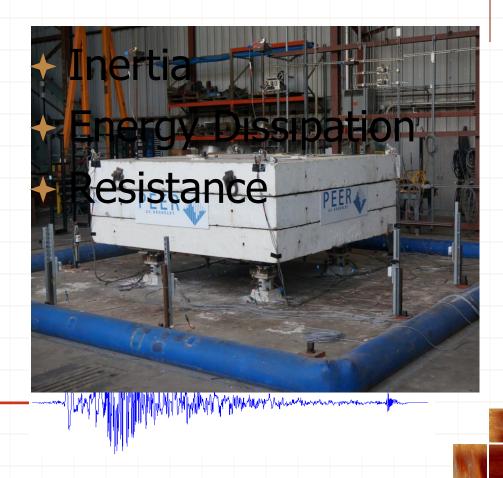




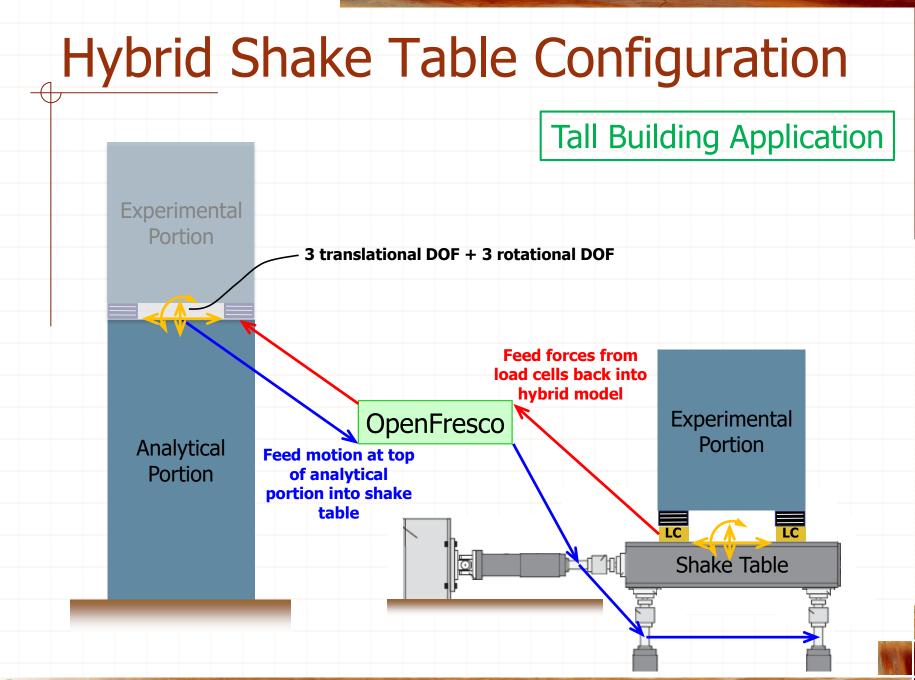
Hybrid Shake Table Testing

 $\mathbf{M} \cdot \ddot{\mathbf{u}} + \mathbf{C} \cdot \dot{\mathbf{u}} + \mathbf{P}_{\mathbf{r}}(\mathbf{u}, \dot{\mathbf{u}}, \ddot{\mathbf{u}}) = \mathbf{P}(t)$





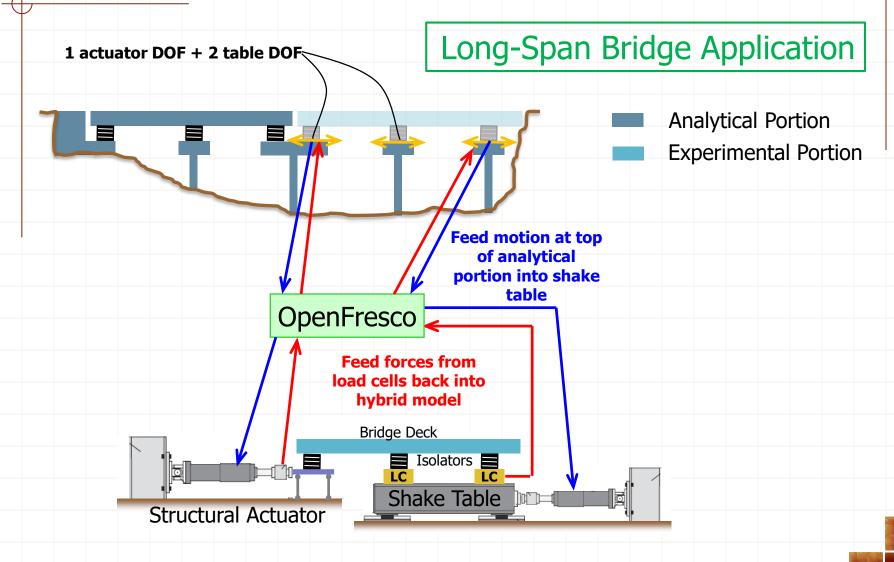






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Hybrid Shake Table Configuration





Equations of Motion

- 1. Slow test
 - $\mathbf{M}\ddot{\mathbf{U}}_{i+1} + \mathbf{C}\dot{\mathbf{U}}_{i+1} + \mathbf{P}_{\mathbf{r}}^{A}(\mathbf{U}_{i+1}, \dot{\mathbf{U}}_{i+1}) + \mathbf{P}_{\mathbf{r}}^{E}(\mathbf{U}_{i+1}) = \mathbf{P}_{i+1} \mathbf{P}_{\mathbf{0}, i+1}$
 - 2. Rapid test
 - $\mathbf{P}_{\mathbf{r}}^{E}\left(\mathbf{U}_{i+1}\right) = \mathbf{P}_{\mathbf{r},i+1}^{E} \mathbf{M}^{E} \, \ddot{\mathbf{U}}_{i+1}^{E} \mathbf{C}^{E} \, \dot{\mathbf{U}}_{i+1}^{E}$
- 3. Real-time test
- $\mathbf{M}^{A} \ddot{\mathbf{U}}_{i+1} + \mathbf{C}^{A} \dot{\mathbf{U}}_{i+1} + \mathbf{P}_{\mathbf{r}}^{A} \left(\mathbf{U}_{i+1}, \dot{\mathbf{U}}_{i+1} \right) + \mathbf{P}_{\mathbf{r}}^{E} \left(\mathbf{U}_{i+1}, \dot{\mathbf{U}}_{i+1}, \ddot{\mathbf{U}}_{i+1} \right) = \mathbf{P}_{i+1} \mathbf{P}_{\mathbf{0}, i+1}$
 - $\mathbf{P}_{\mathbf{r}}^{E}\left(\mathbf{U}_{i+1}, \dot{\mathbf{U}}_{i+1}, \ddot{\mathbf{U}}_{i+1}\right) = \mathbf{P}_{\mathbf{r}, i+1}^{E} + \mathbf{M}^{E} \ddot{\mathbf{U}}_{i+1}$
 - 4. Smart shaking table test
 - $\mathbf{P}_{\mathbf{r}}^{E}\left(\mathbf{U}_{\mathbf{t},i+1},\dot{\mathbf{U}}_{\mathbf{t},i+1},\ddot{\mathbf{U}}_{\mathbf{t},i+1}\right) = \mathbf{P}_{\mathbf{r},i+1}^{E} + \mathbf{M}^{E}\ddot{\mathbf{U}}_{\mathbf{t},i+1}$



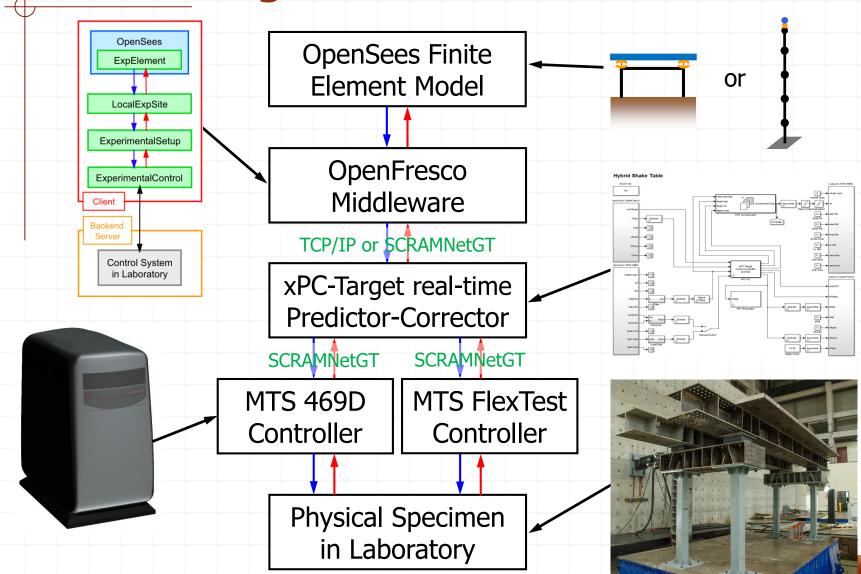
Important Analysis Parameters

- OpenSees or OpenSeesSP as comp. driver
- + Using AlphaOSGeneralized ($\rho_{inf} = 0$)
- Next time try KRAlphaExplicit method
- No iterations necessary
- Using MultipleSupport excitation pattern in OpenSees to get absolute response

 ← Gravity loads on test specimen always present → apply gravity loads to numerical portion before connecting with shake table + apply disp. commands relative to start of test



Connecting to MTS 469D + FlexTest

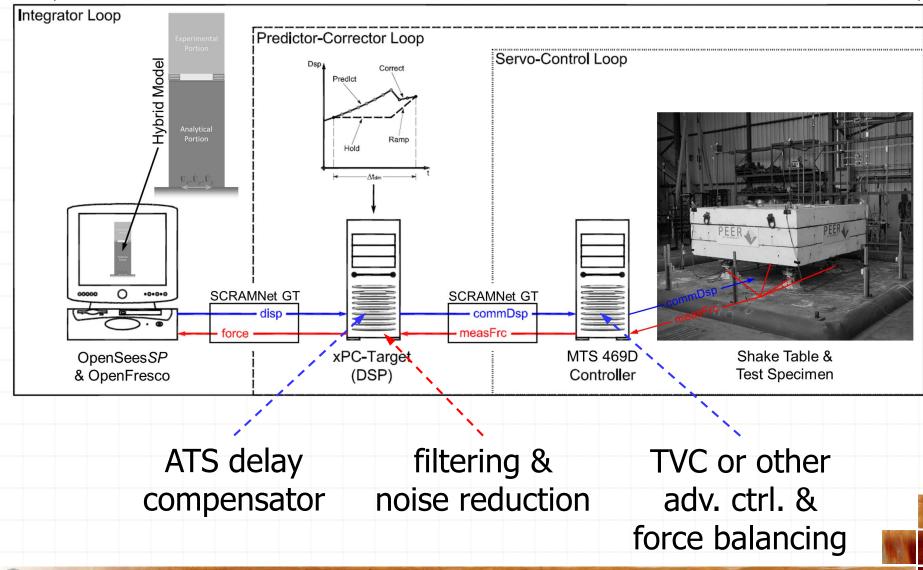




Improving Stability & Accuracy

- Delay compensation is essential for realtime hybrid simulations (RTHS)
- Use Adaptive Time Series (ATS) delay compensator (by Y. Chae)
- Modify ATS to use target velocities and accelerations computed by predictorcorrector algorithm instead of taking derivatives of target displacements
 Use stabilization and loop-shaping
 Sensor noise reduction by filtering fbk

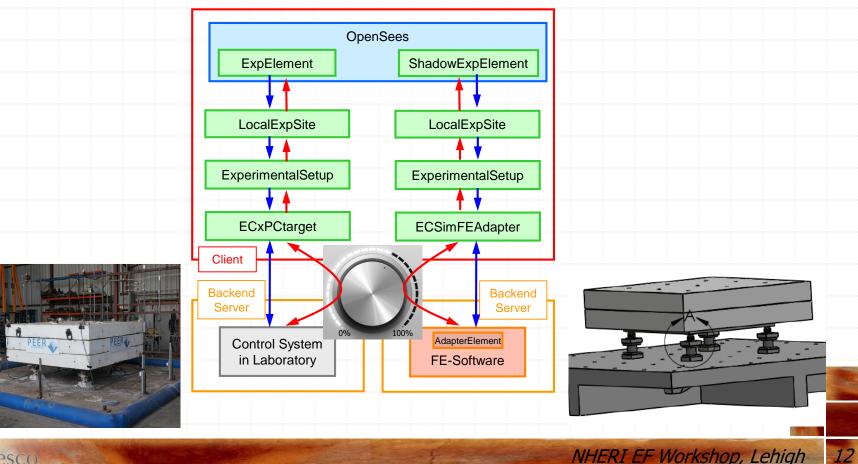
Three-loop architecture





Test Rehearsal

 Use FE-Adapter element method to simultaneously connect hybrid model to a numerically simulated test specimen



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Safety Precautions

At analysis side

- Set limit on displacement command (saturation and possibly rate limit)
- Set limit on actuator force so that once the limit is exceeded, the analysis model sends displacement commands to ramp both table and actuator to starting positions

At controller side

 Set both displacement and force limits so that once the limit is exceeded, the actuator pressure is switched to low, therefore, limiting the actuator force that can be applied to the specimen



Bridge Application





Shake Table + Structural Actuator



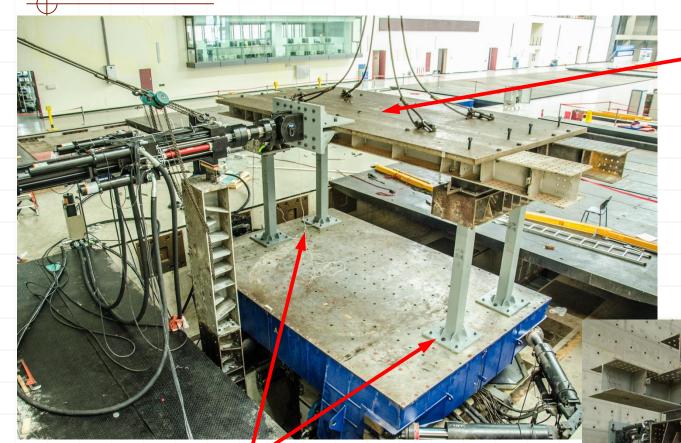


Hybrid Model Development experimental bridge with partial bridge deck weight Remaining numerical mass ExpBridge S

Actual Bridge Configuration (with foundation + soil) Simplified Hybrid OpenSees Model of Bridge (Stage 2)



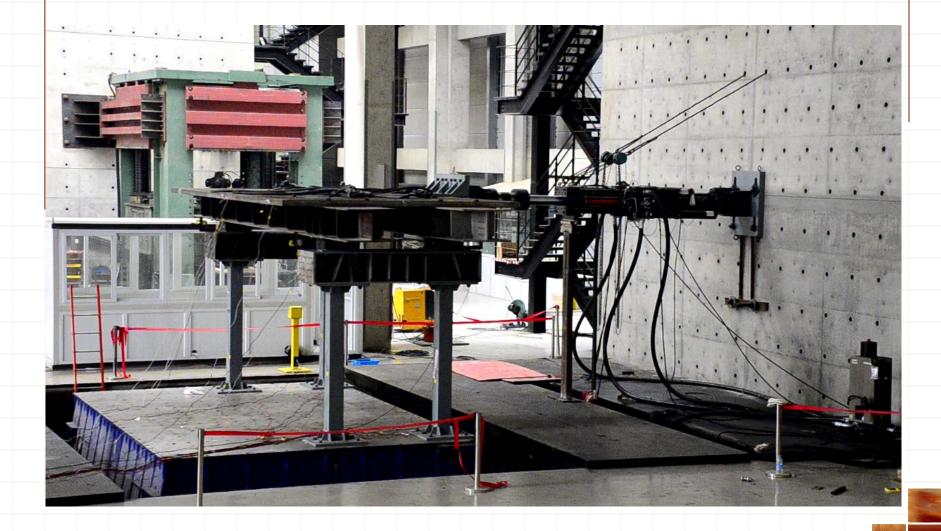
Experimental Setup



Partial-weight bridge deck

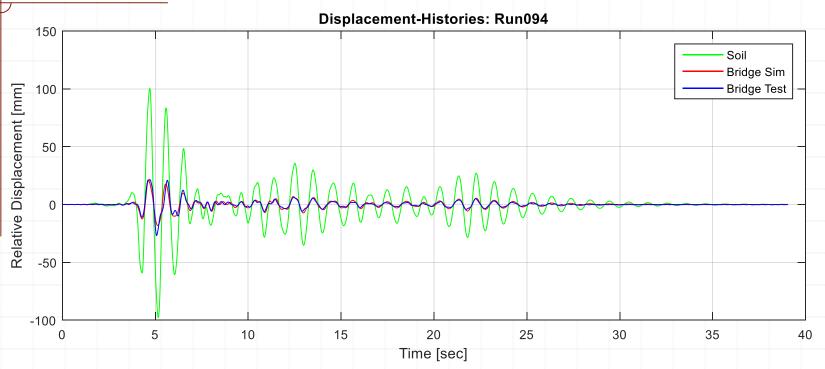
Using table observer to get shear forces at bottom of columns (load cells would be better)

Movie of Test





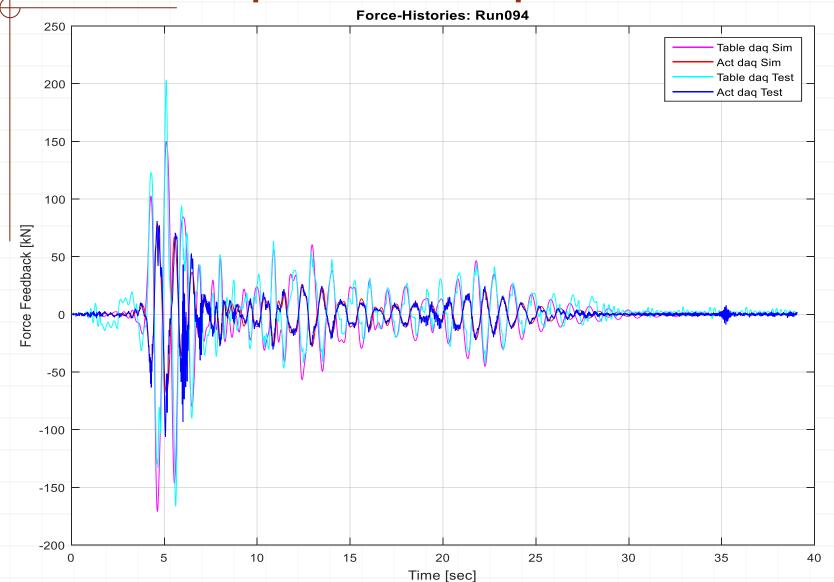
Displ. Response Comparison



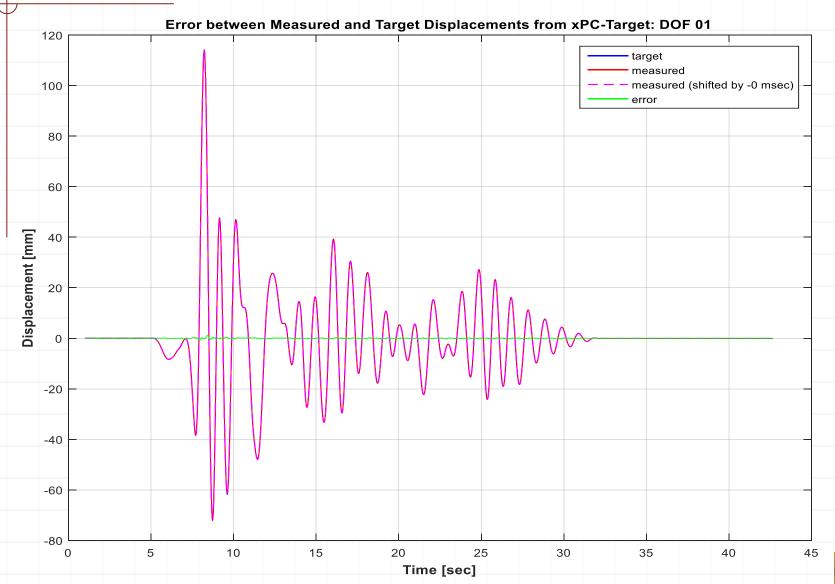
Accuracy is assessed using

- FFTs of tracking error
- Tracking Indicator (by Mercan and Ricles)
- RMS Error histories
- Comparison with purely numerical simulation

Force Response Comparison









Building Application

PFF





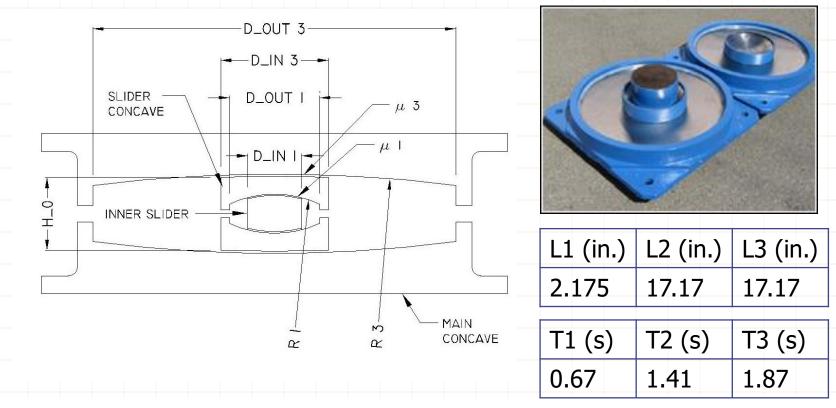
PEER Shake Table Facility

- 20 ft x 20 ft table size
- Still the largest 6 DOF shake table in the US
- Can test structures, weighing 100,000 lbs, to horizontal accelerations of 1.5 g
- +/- 5 in. horizontal displacement capacity
- +/- 2 in. vertical displacement capacity
- +/- 40 in./sec velocity capacity



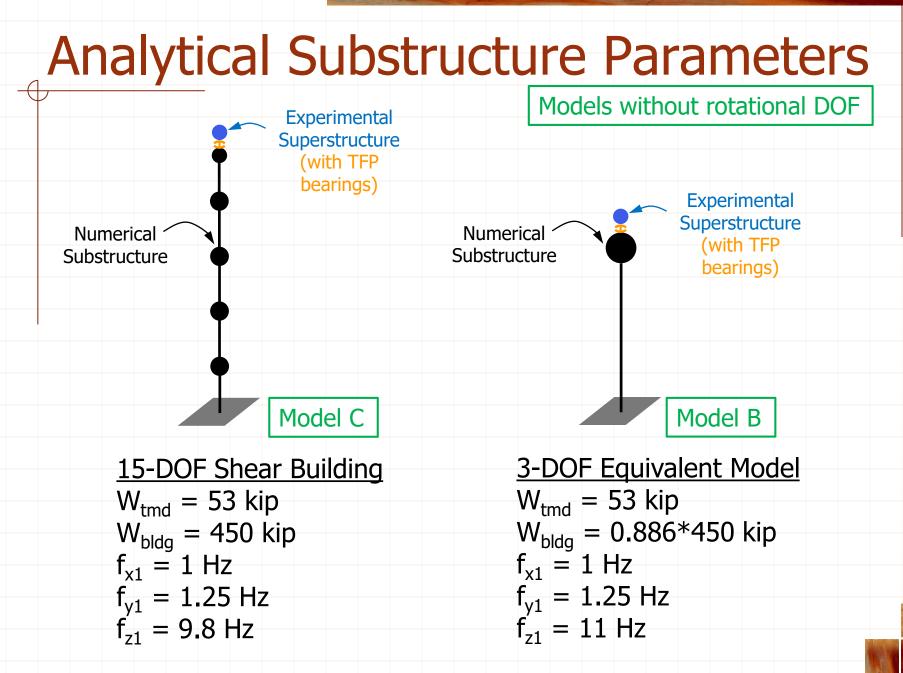


Triple Friction Pendulum Bearings

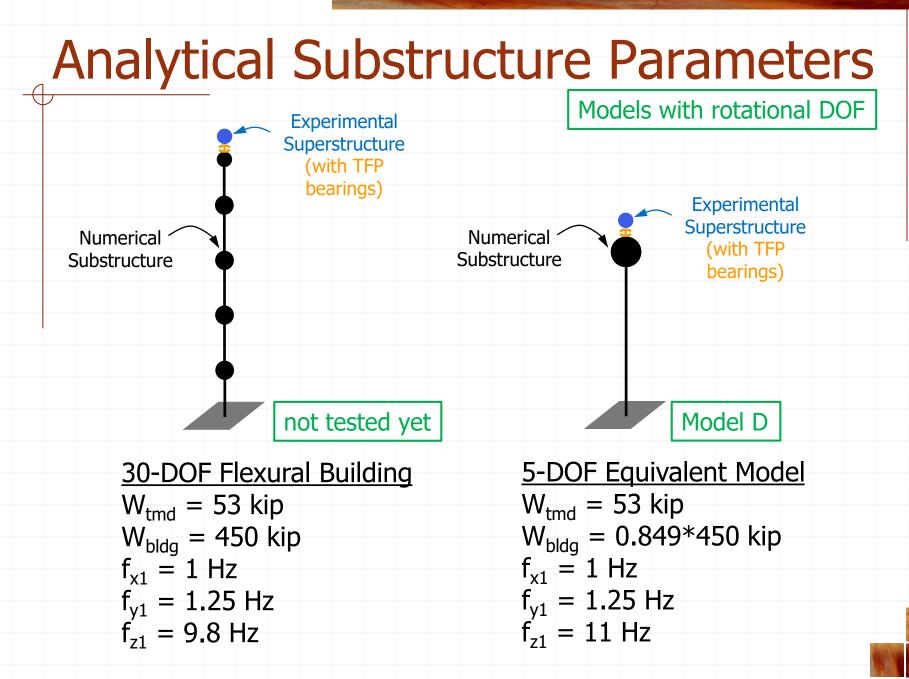


	Inner sliding surfaces	Outer sliding surfaces
Dish radius (inch)	3	18.64
Height (inch)	1.65	2.94
Outer diameter (inch)	2.60	9
Inner diameter (inch)	1.75	3





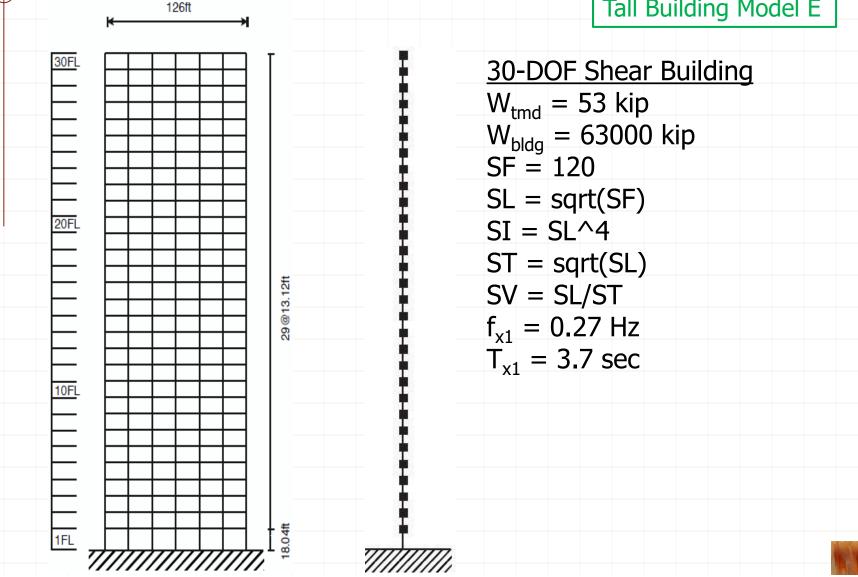






Analytical Substructure Parameters

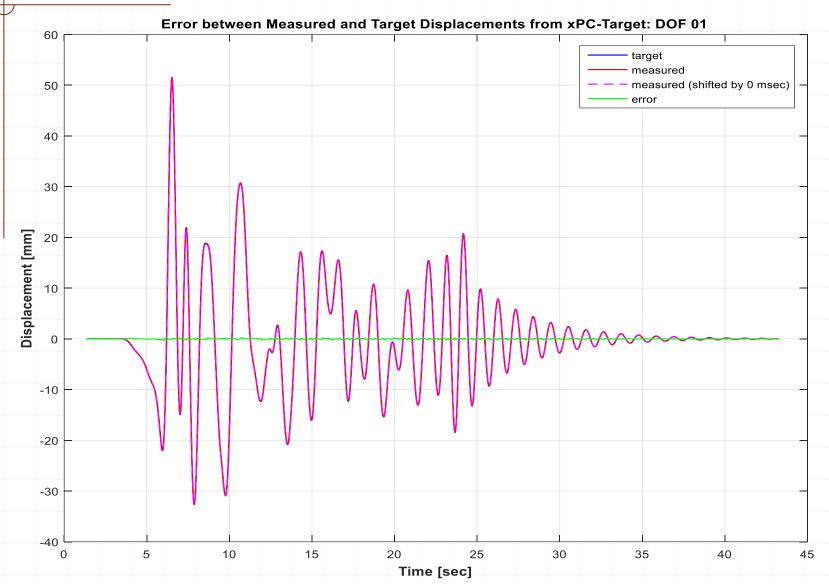
Tall Building Model E



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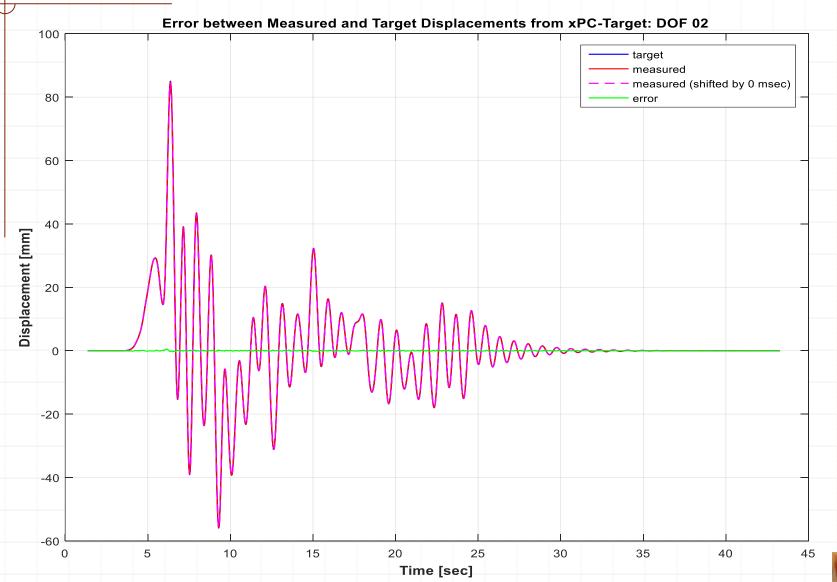




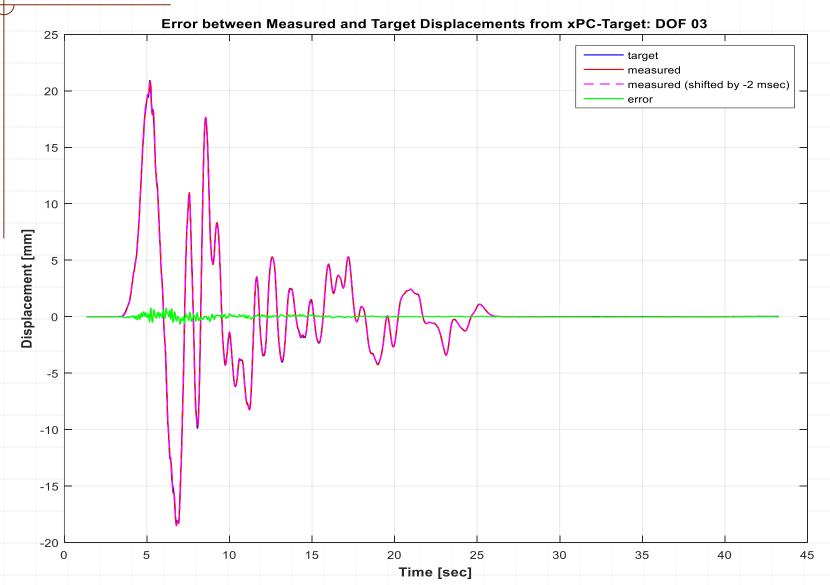


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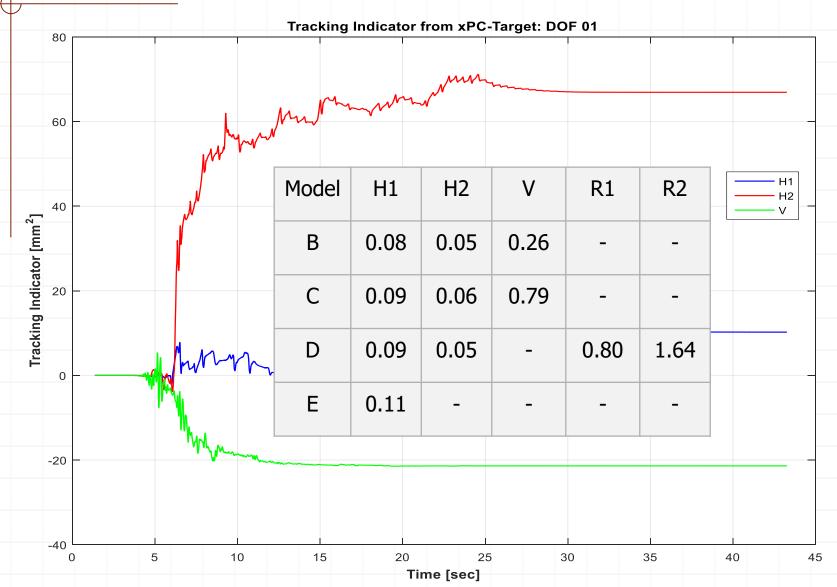


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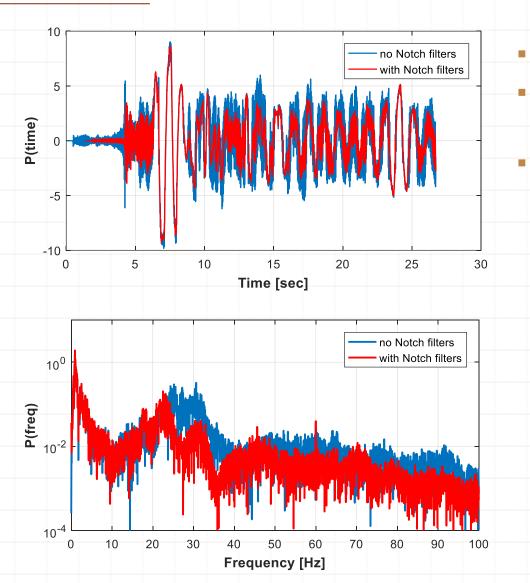


Tracking Indicator & NRMSE[%]





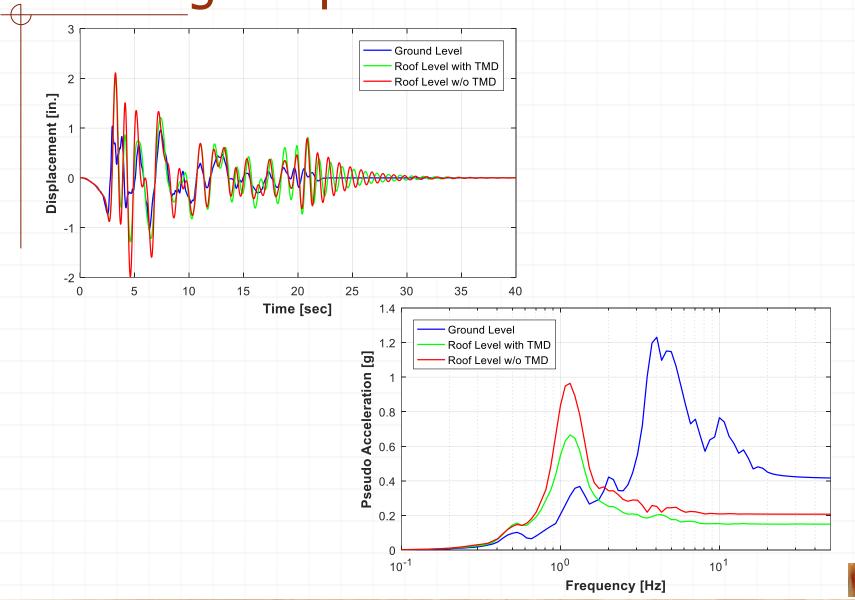
Filtering of Force Feedback

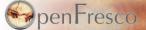


Future work required Investigate other filtering techniques Investigate Kalman filtering techniques (can this be applied to force feedbacks using an predictive analysis model in parallel?)



Building Response Modification





Summary & Conclusions

- Ability to drive a MDOF shake table through a finite element model
- Shake table platform can thus represent a floor or the roof of a building, the motion on top of a bridge column, or the ground surface on top of a soil domain
- Performed large-scale RTHS where a shake table is combined with a dynamic structural actuator applied to a bridge
- Ability to perform parameter studies

Summary & Conclusions

 Use whenever the dynamics of the test specimen significantly affects the response of the supporting structure or soil and, therefore, alters the required input to the shake table as testing progresses

ATS delay compensator worked very well

 Need to further investigate sensor noise reduction methods to improve feedback signals (look into Kalman filters)



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Questions? Thank you!

http://openfresco.berkeley.edu



